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| 14. ABSTRACT<br>Recent advances in the development of highly conductive ionic liquids have made them of interest for use as propellant in spacecraft propulsion systems. Electrospray thrusters apply strong electrostatic fields to an ionic liquid in order to extract and accelerate charged particles/droplets, producing thrust. The behavior of these ionic liquids as they pass through the components of an electrospray system can have a significant effect on thruster operation. The wetting and adhesion behavior between the ionic liquid propellant and solid materials can be characterized using the surface tension and contact or 'wetting' angle formed when a liquid droplet comes in contact with a solid surface. Ideally this angle is a function of the interactions between the solids surface energy, the surface tension of the liquid and the interactions of both with the surrounding medium. Deviation from ideal contact angle behavior can indicate surface inconsistencies, environmental effects or contamination of the solid and liquid. Contact angle and surface tension measurements are presented for the ionic liquid propellant 1-Ethyl-3- methylimidazolium bis(triuroromethylsulfonyl)imide, called EMIIm or EtMeImTf2N, with respect to various substrate materials and environmental conditions. Analysis of these measurements determines optimum materials and operating conditions for current and future electrospray thruster designs. |                                 |                                  |   |  |  |
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California State University  
**Northridge**

# **EMIIM WETTING PROPERTIES & THEIR EFFECT ON ELECTROSPRAY THRUSTER DESIGN**

**March 2012**

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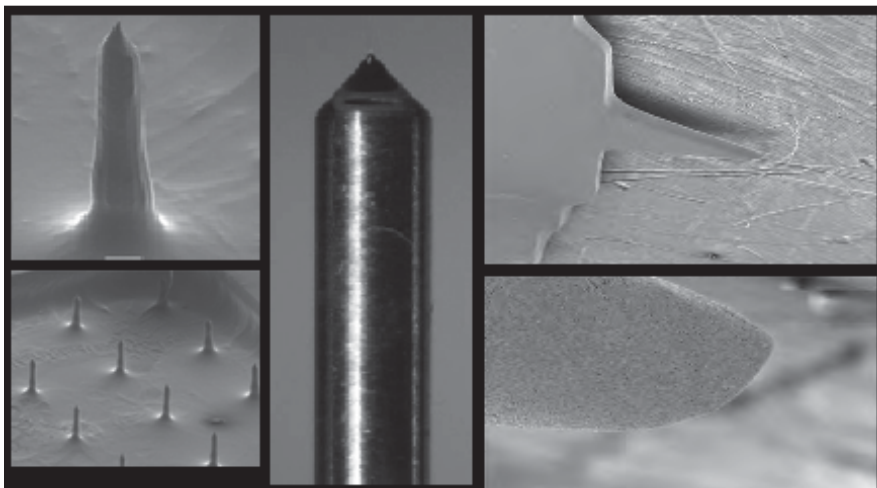
## Motivation & Objective

- **Electrospray thruster for LISA Pathfinder - DRS Payload**
  - Thruster failure mechanisms identified as dependant on wetting characteristics of propellant & component materials
  - Wetting data needed to model these mechanisms & possible mitigation techniques
- **Process for measuring amount of wetting**
  - Develop ideal method for measurement
  - Determine uncertainties in measurement
  - Test other ionic liquid (IL) propellants (BMIBG4, Air Force formulations...)



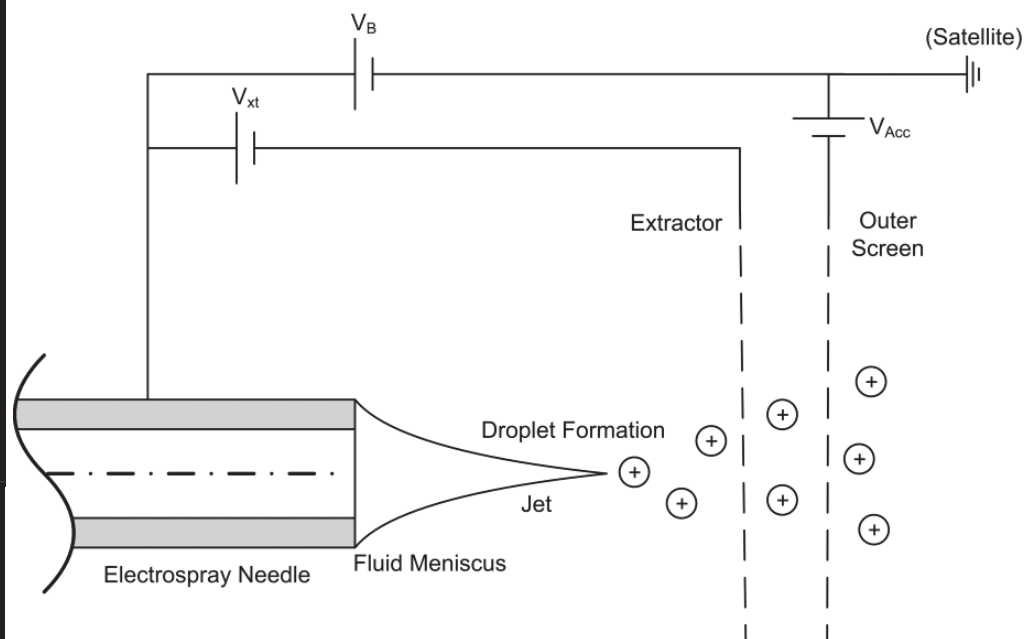
**Determine amount of wetting between thruster / propellant & relationship with failure mechanisms**

# Electrosprays

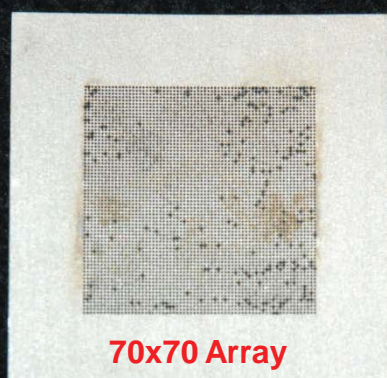


- **Emitter**

- Internally / externally wetted, porous
- Allow propellant transport to tip



Single Aperture



70x70 Array

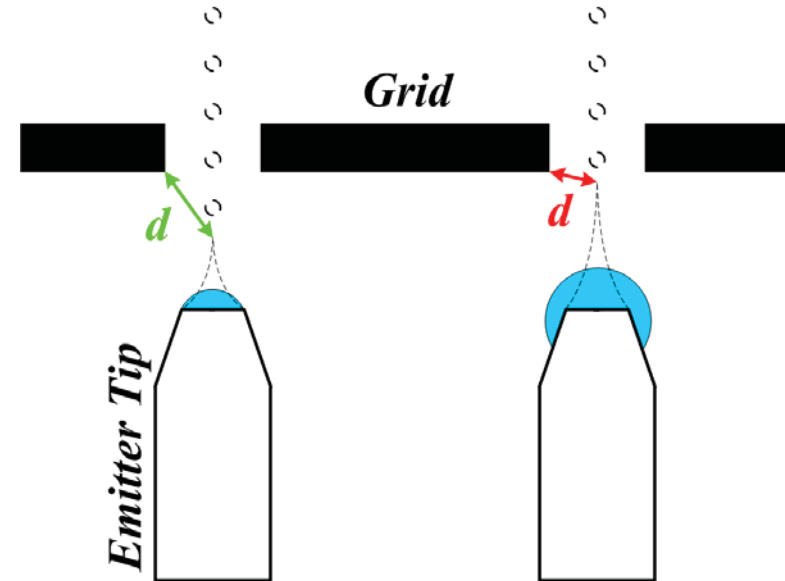
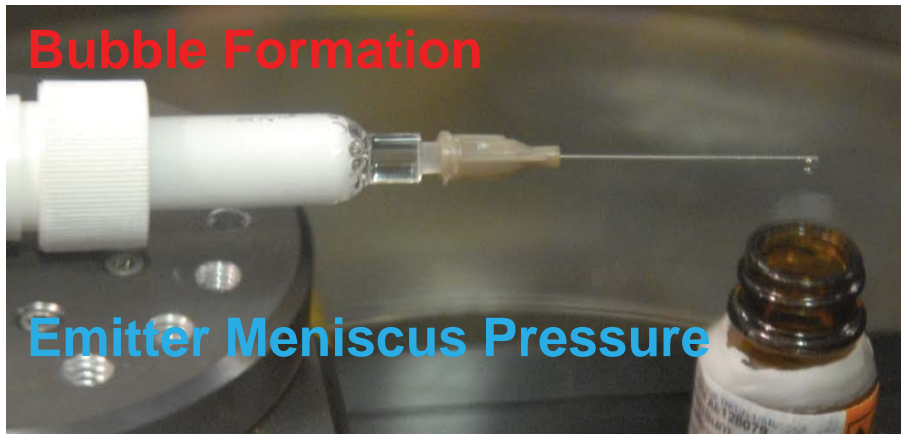
- **Extraction Grid**

- Apply Lorentz force to propellant
- Extract ions / droplets depending on polarity

- **Acceleration Grid**

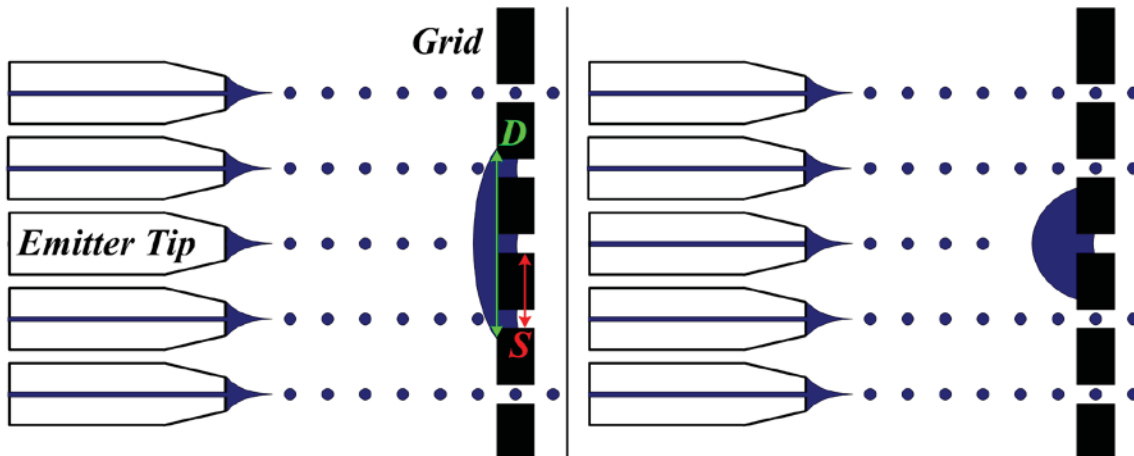
- Increase velocity of particles

# Failure Mechanisms



**Grid Obstruction**  
**Grid Wetting Angle**

**Arcing Between Grid & Emitter**



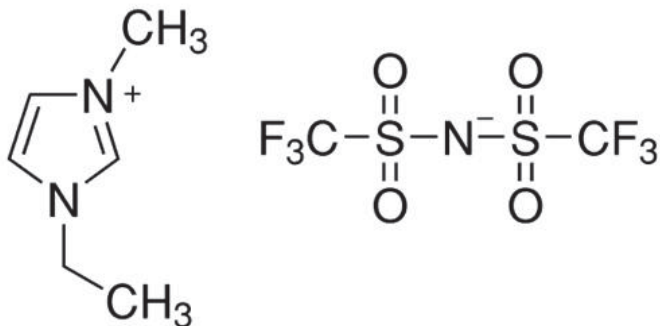
**Emitter Tip Wetting**

**Failure Mechanism**  
**Possible Wetting Solution**



## Electrospray Propellant

- High conductivity / charge to mass ratio
- Negligible vapor pressure
- Low Viscosity



| Property                             | Value                | Units              |
|--------------------------------------|----------------------|--------------------|
| Density (~20°C)                      | 1523.6               | kg·m <sup>-3</sup> |
| Surface Tension                      | 38.1                 | J·m <sup>-2</sup>  |
| Expansion Coefficient ( $\alpha_p$ ) | $6.47 \cdot 10^{-6}$ | K <sup>-1</sup>    |
| Critical Temperature                 | 1127                 | K                  |
| Vapor Pressure                       | Negligible           | -                  |

## Test Fluid

- Supplied by Strem Chemicals Inc. (CAS# 174899-82-2)
- Factory sealed with dry nitrogen
- Water content (Karl-Fischer Titration)
  - Factory Sealed Container: 2411±41 ppm
  - Waste EMIm exposed to ambient conditions for ~8 months: 2825 ±16 ppm
  - Hygroscopic & Hydrophobic



## 1-Ethyl-3-methylimidazolium bis(trifluoromethylsulfonyl)imide

# Wetting Theory

## Idealized System:

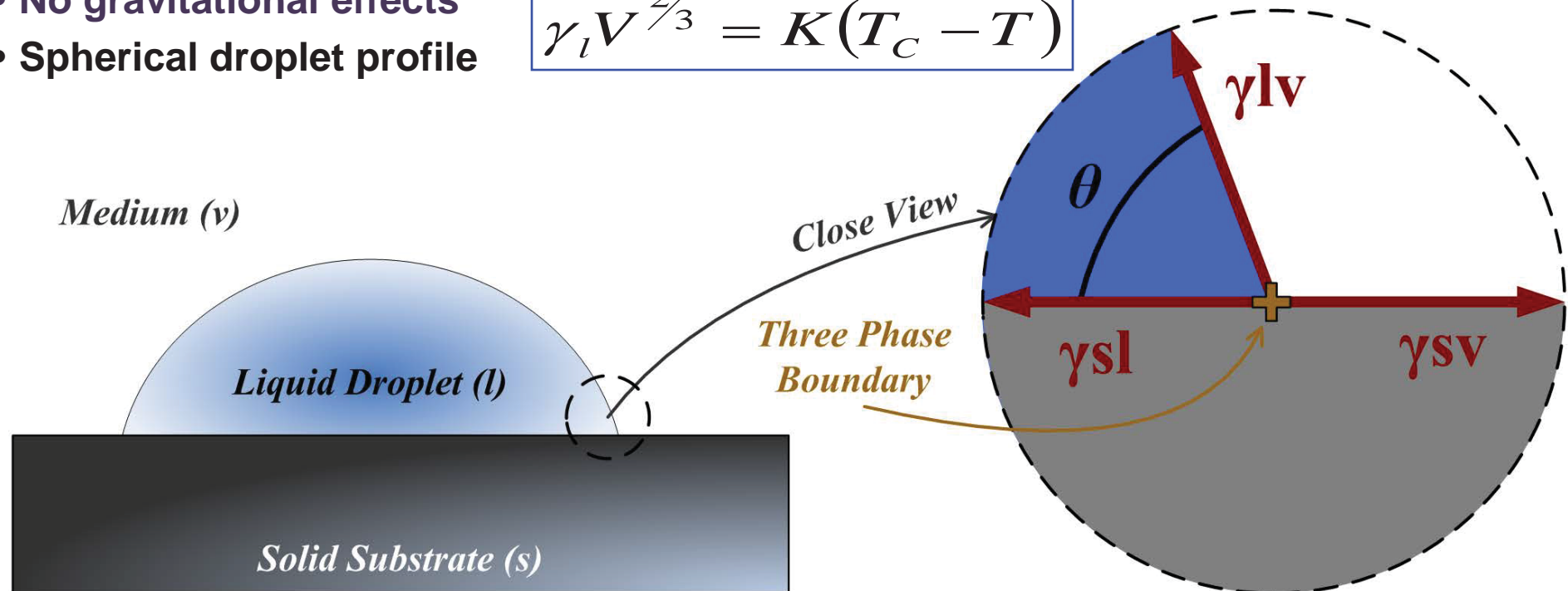
- **Smooth ( $Ra = 0$ )**  $\boxed{\cos(\theta') = r_s \cos(\theta)}$
- **No chemical Reaction, inert components**
- **No impurities present**  $\boxed{\theta' = kt^n}$
- **Chemically homogeneous components**
- **Constant temperature/pressure**
- **No gravitational effects**
- **Spherical droplet profile**

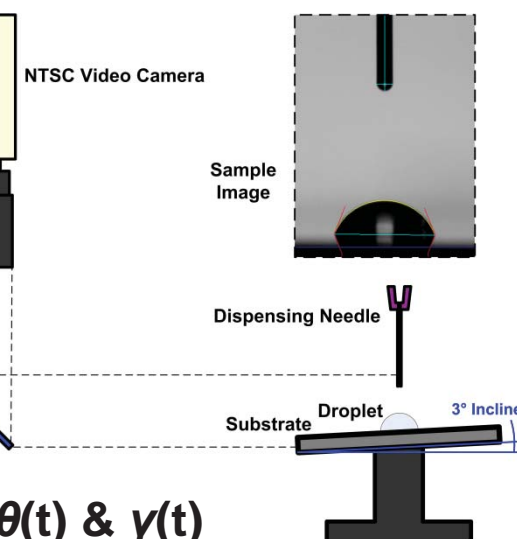
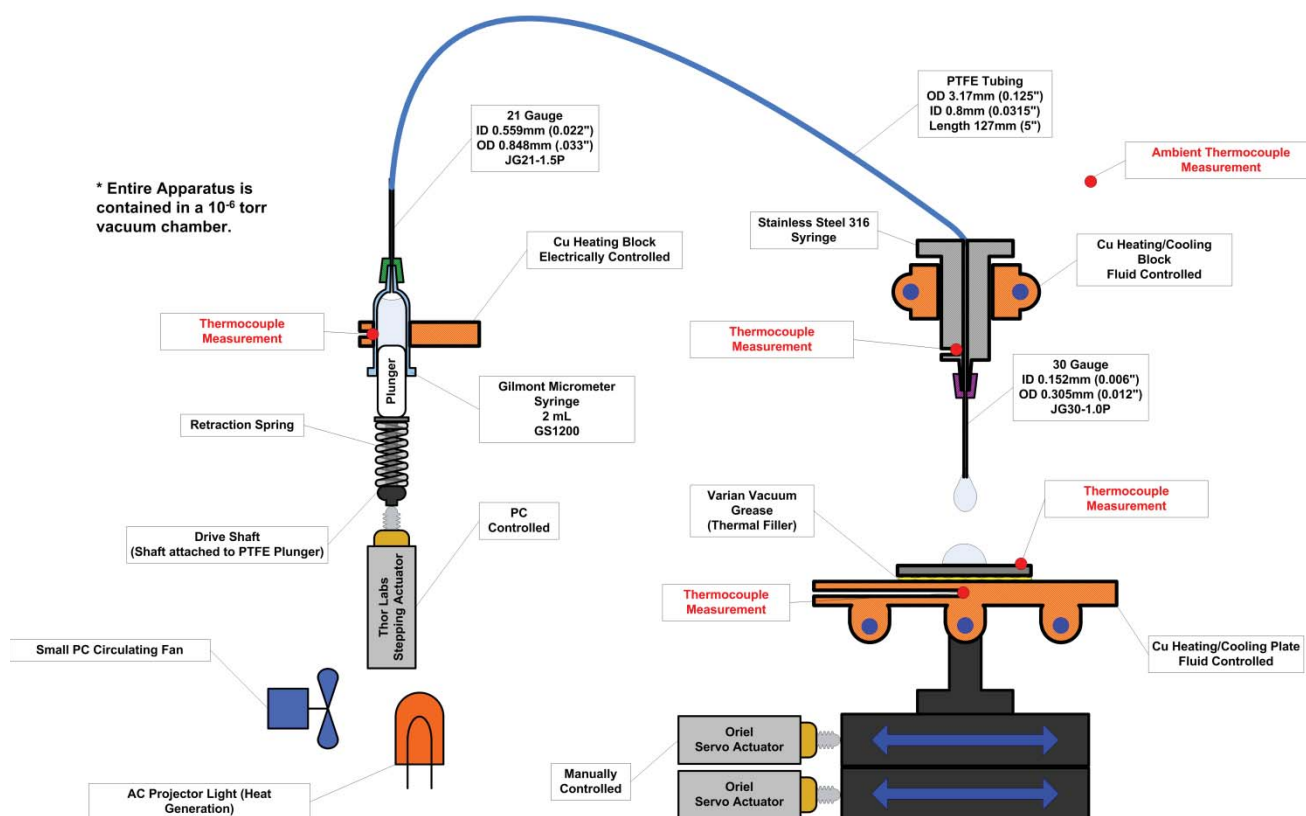
## Young's Equation

$$\cos(\theta) = \frac{\gamma_s - \gamma_{sl}}{\gamma_l} = \frac{\pi_{sl}}{\gamma_l}$$

## Eotvos

$$\gamma_l V^{2/3} = K(T_C - T)$$





## Chamber 8, AFRL Edwards AFB

- Two stage pump train ( $10^{-6}$  Torr)

## First Ten Angstroms (FTA125)

- Real time Sessile/pendant drop recording
- FTA32 analysis software, time resolved measurements:  $\theta(t)$  &  $\gamma(t)$



- Simulate On-Orbit Electrospray Environment
- Determine Optimal Materials & Conditions



**Surface Tension  
Verify System**



**Surface Tension  
Temperature**



**Surface Tension  
Pressure**



**Contact Angle  
Equilibrium**



**Contact Angle  
Temperature**

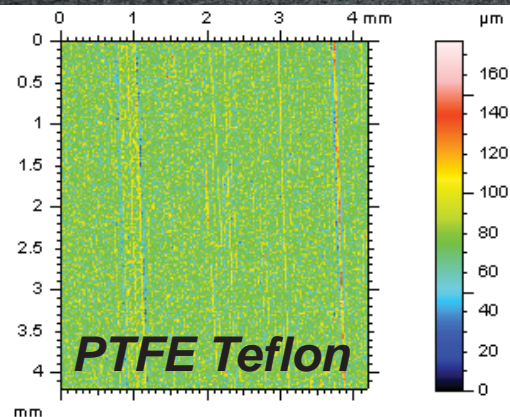
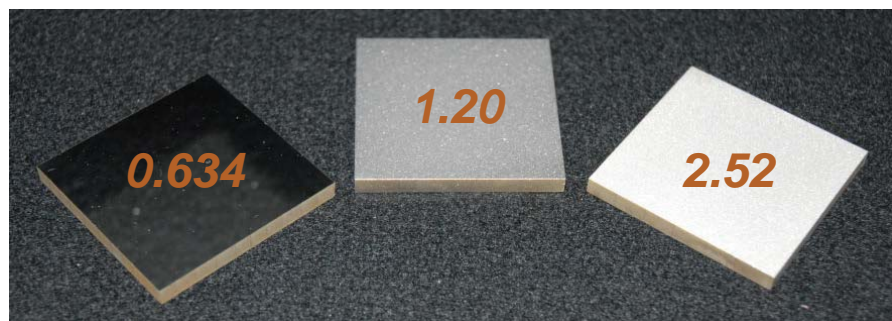


**Contact Angle  
Pressure**



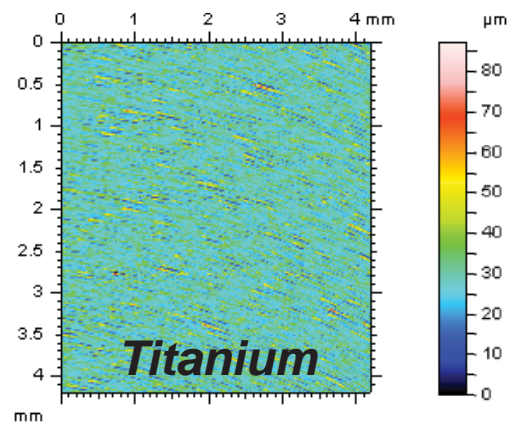
**Contact Angle  
Advancing/Receding**

# Substrates

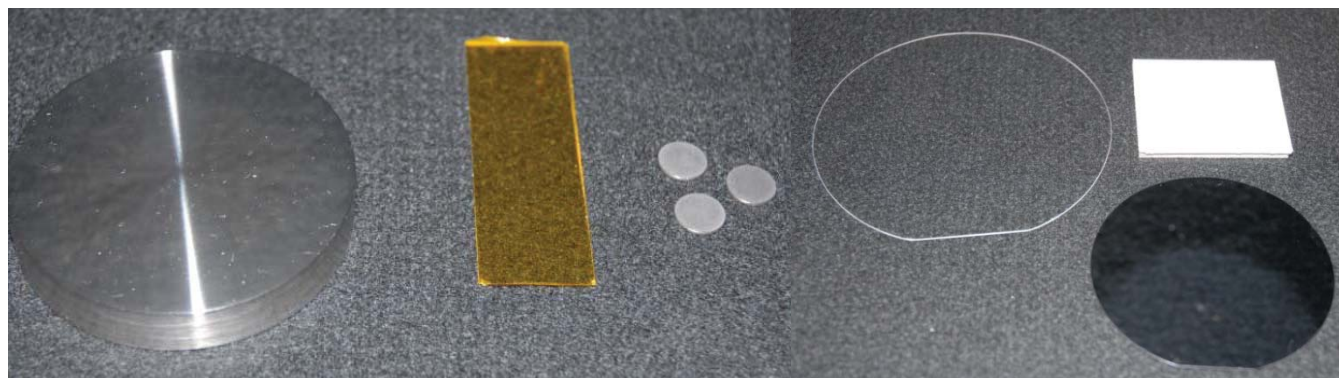


•*Ra Measured with an optical laser profilometer*

•*Limited resolution for smooth finishes*

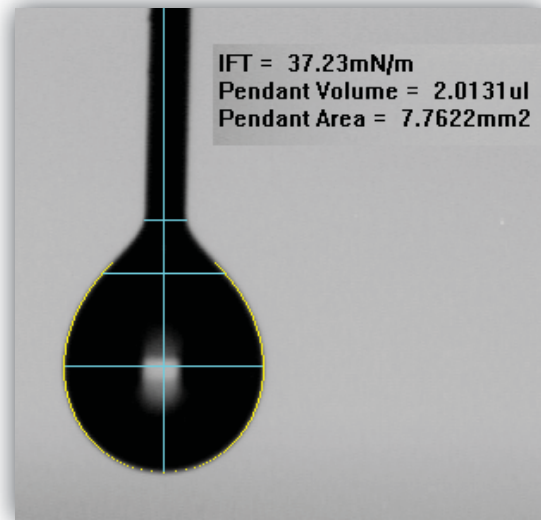


| Material     | Thickness (mm) | Ra (μm)         |
|--------------|----------------|-----------------|
| SS316        | 4.7            | 0.634/1.20/2.52 |
| Fused Silica | 0.5            | < 0.144         |
| Glass        | 1              | < 0.144         |
| Kapton       | 0.05           | 0.144           |
| PTFE Teflon  | 1.38           | 1.47            |
| Pyrex        | 13             | < 0.144         |
| Tungsten     | 1              | 0.351           |
| Silicon      | 0.5            | < 0.144         |
| Titanium     | 13             | 0.600           |



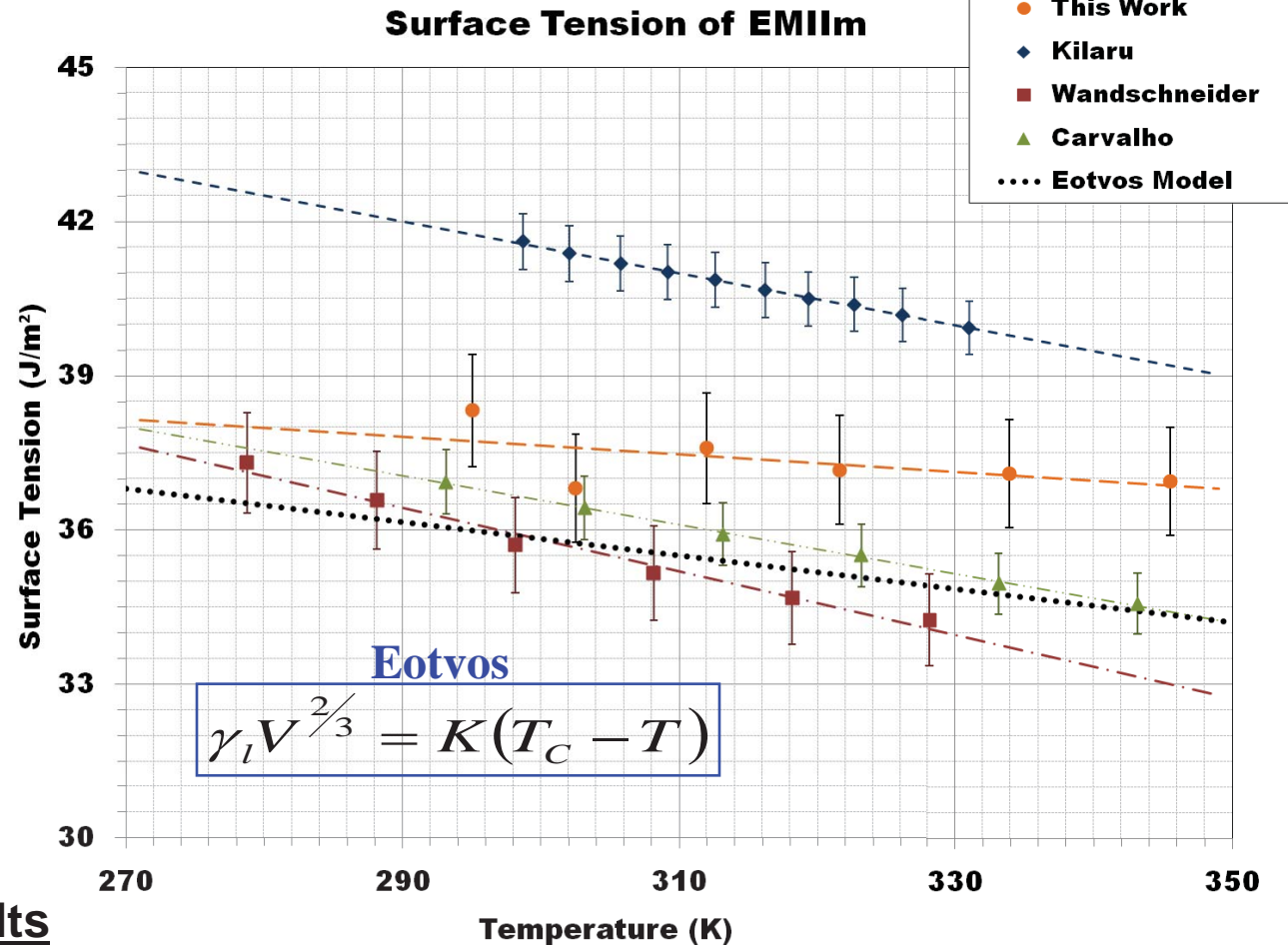


# Surface Tension I



$$\gamma_l = 38.1 \pm 1.09$$

(~25°C, 1 ATM)



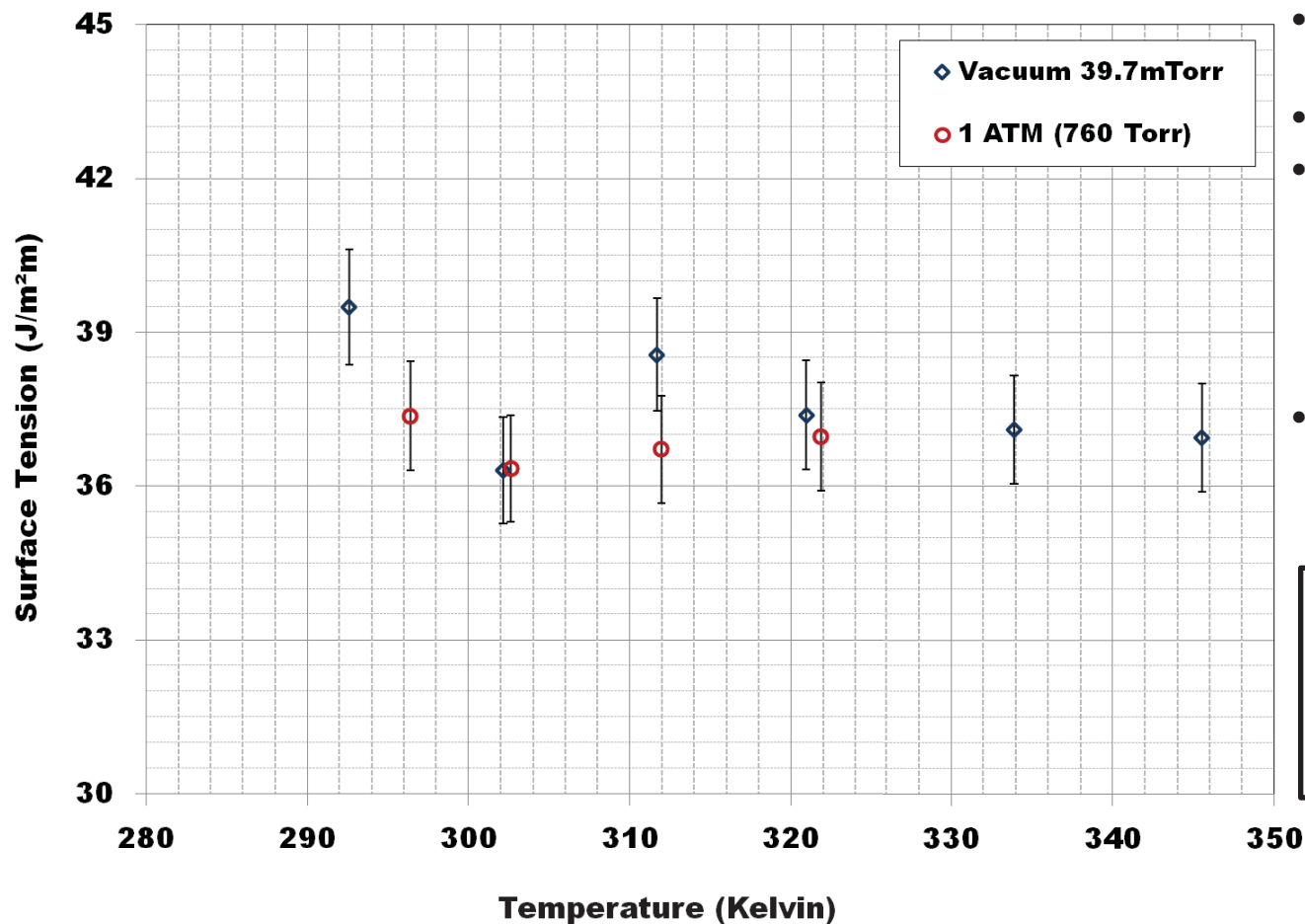
## Surface Tension ( $\gamma_l$ ) Results

- 20 measurements taken at each temperature (T)
- Reasonable agreement with contemporary research / Model
- Decreasing  $\gamma_l$  as T increases »  $\theta$  should decrease as well

# Surface Tension II



**EMIIIm Surface Tension**



## Surface Tension ( $\gamma$ ) Results

- 8 measurements taken at each temperature (T) / Pressure (P)
- No meaningful trend measured
- Likely that properties change:
  - Very small change with (P)
  - Near transition state (high-T / low-P)
- Change not measurable with this apparatus

**Two pressures tested:**

**Ambient 760 Torr**

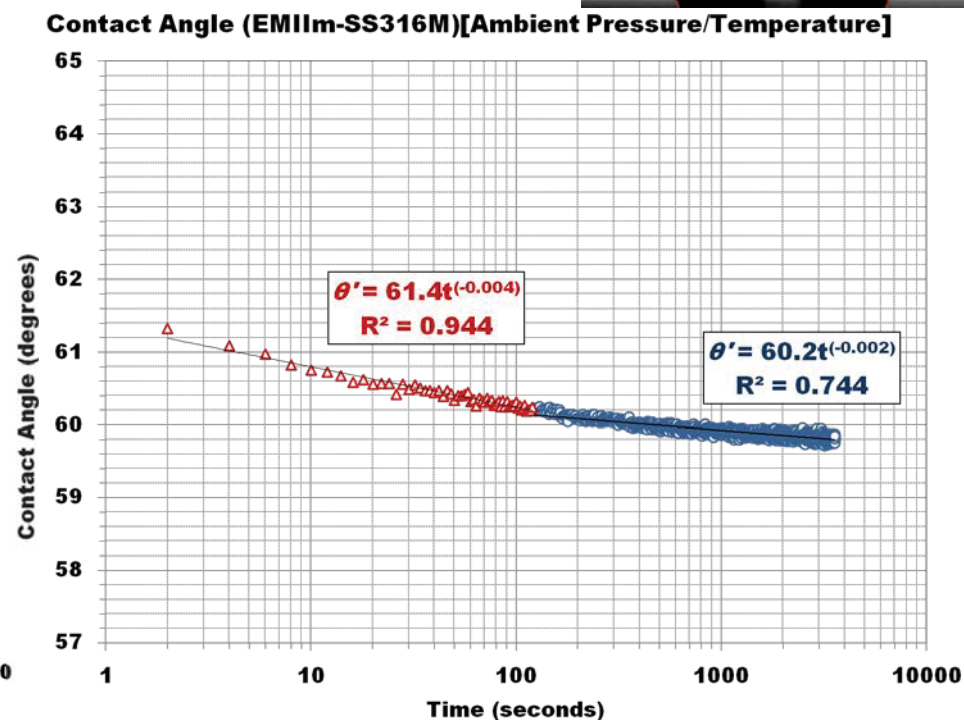
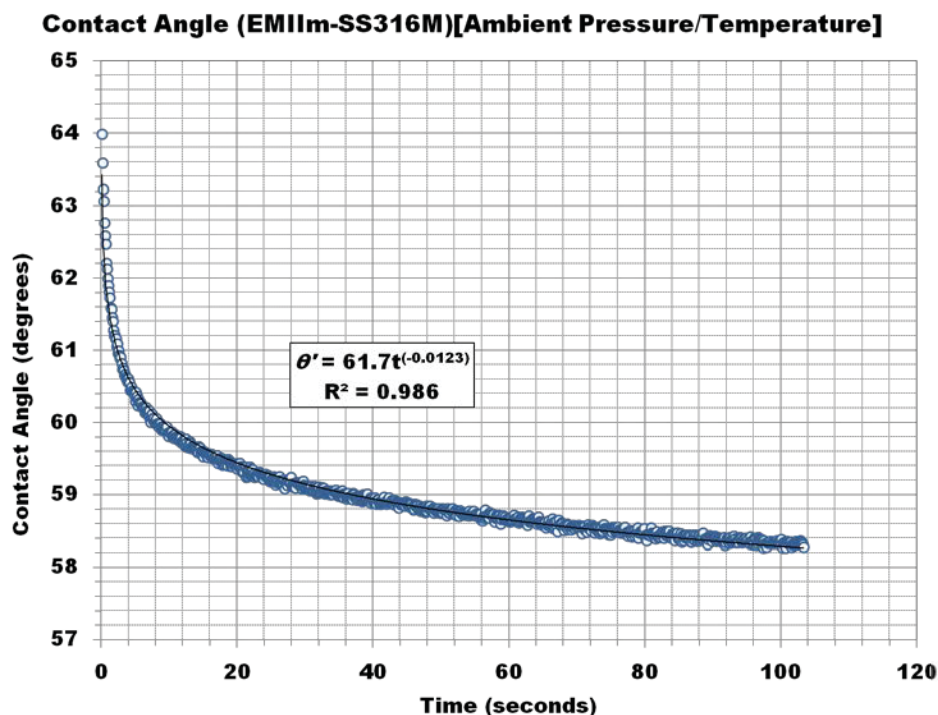
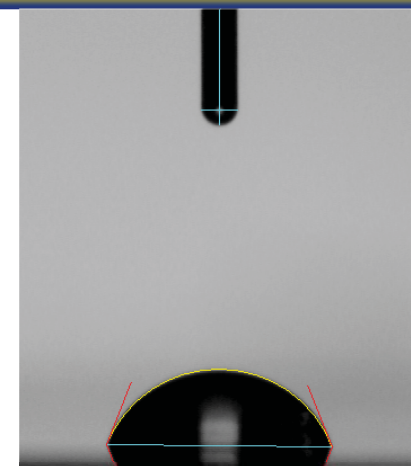
**Vacuum 40 mTorr**



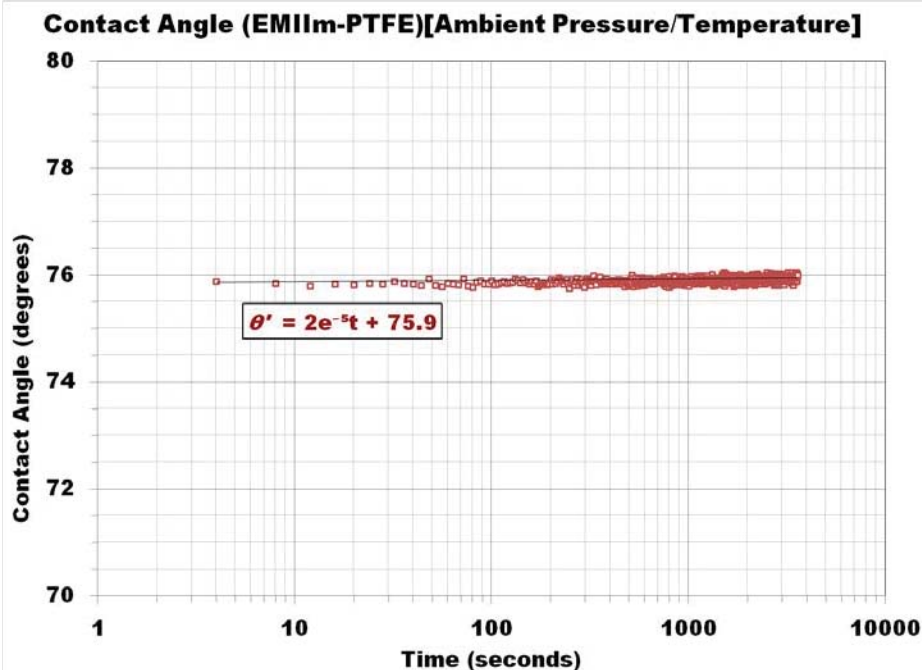
## Dynamic Angle Behavior over Time

- Indicative of chemical reaction between component-contaminants (Marmur et. al. / Kwok)
- Unstable angle follows power law over time
- Coefficients recorded for each substrate, varying T & P
  - No measurable change in  $k(T, P)$  or  $n(T, P)$

$$\theta' = kt^n$$





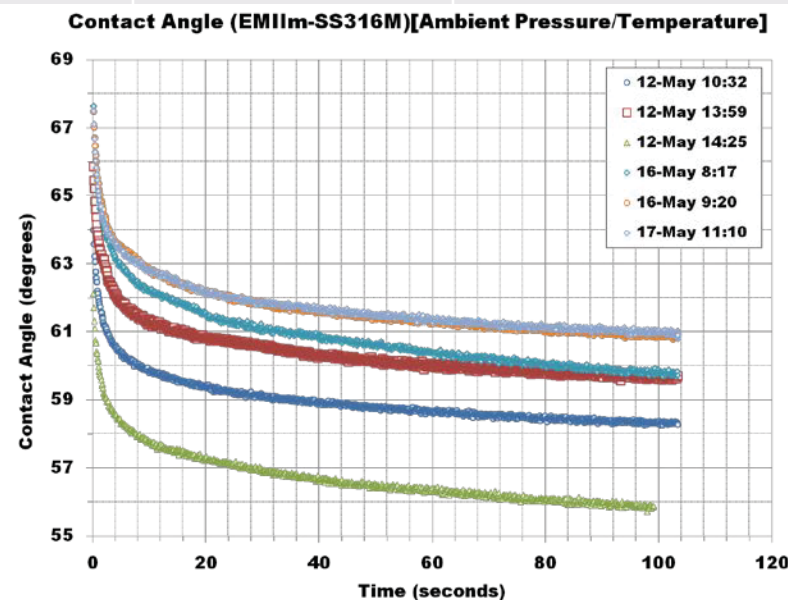


| Material     | $k$                | $n$                     |
|--------------|--------------------|-------------------------|
| SS316        | 57.2 / 60.9 / 55.1 | -0.0055/-0.0104/-0.0285 |
| Fused Silica | 57.9               | -0.0281                 |
| Glass        | 45.6               | -0.0014                 |
| Kapton       | 59.3               | -0.0079                 |
| Pyrex        | 45.8               | -0.0336                 |
| Tungsten     | 39.1               | -0.0015                 |
| Silicon      | 56.4               | -0.0106                 |
| Titanium     | 63.2               | -0.0547                 |

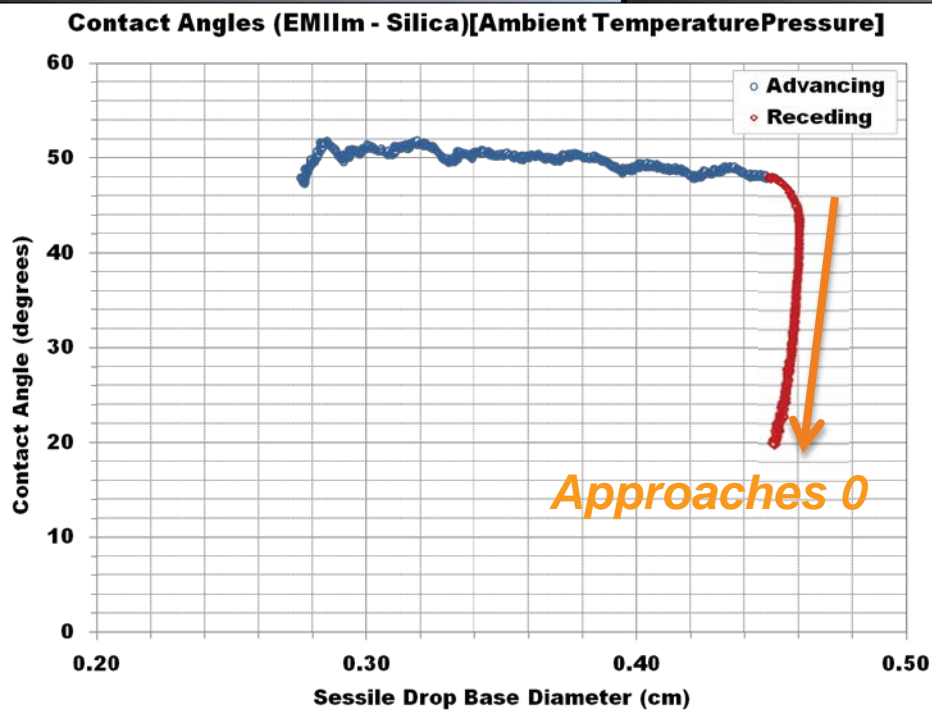
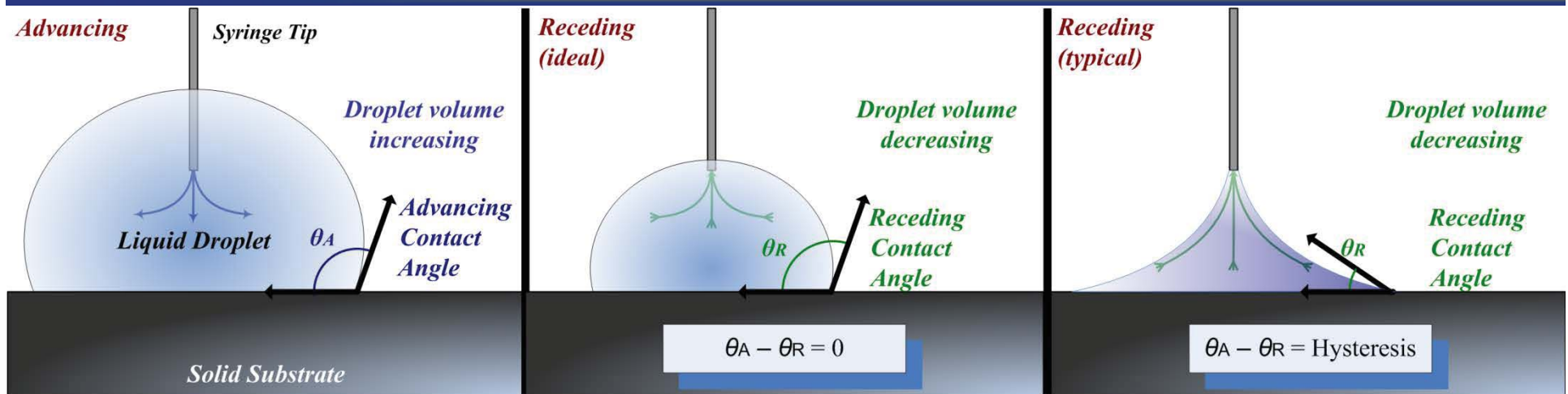
| Material    | $m$               | $b$  |
|-------------|-------------------|------|
| PTFE Teflon | $2 \cdot 10^{-5}$ | 75.9 |

## Equilibrium Contact Angle Results

- Reaction affected each substrate except PTFE
- $k$  appears to indicate initial contact angle
- $n$  indicates rate of spreading
  - Uncertainty between data sets:  $\pm 4^\circ$
- Surface roughness appears to increase wetting

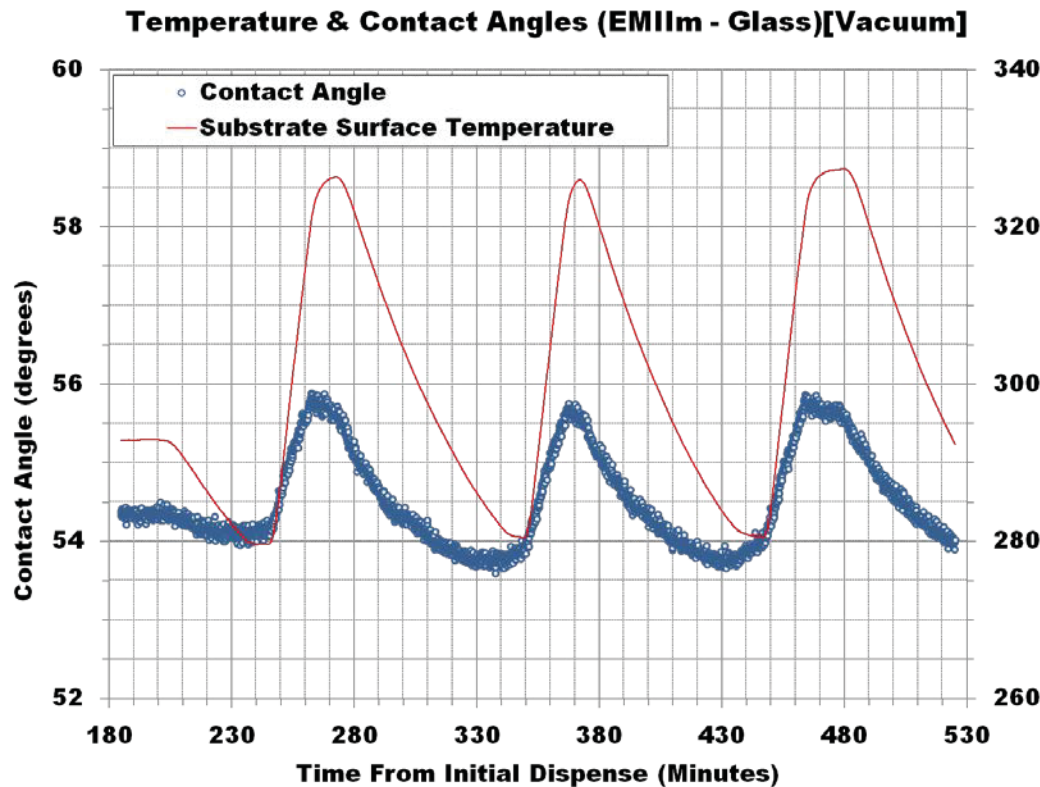


# Advancing / Receding Angles I



| Material     | Advancing          | Receding |
|--------------|--------------------|----------|
| SS316        | 52.1 / 58.2 / 55.9 | 0        |
| Fused Silica | 51.6               | 0        |
| Glass        | 55.2               | 0        |
| Kapton       | 52.3               | 0        |
| Pyrex        | 49.6               | 0        |
| Tungsten     | 43.8               | 0        |
| Silicon      | 48.0               | 0        |
| Titanium     | 52.3               | 0        |
| PTFE         | 68.3               | 56.6     |

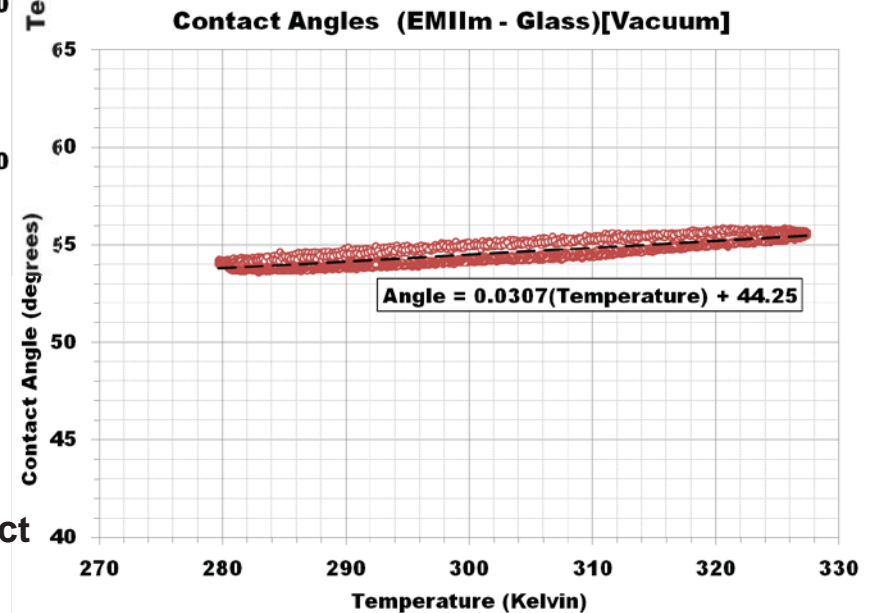
# Temperature Effect



$$T \uparrow \quad \gamma_l \downarrow \quad \theta \uparrow \quad \gg \quad \pi_{sl} \uparrow$$

$$\cos(\theta) = \frac{\gamma_s - \gamma_{sl}}{\gamma_l} = \frac{\pi_{sl}}{\gamma_l}$$

$$\gamma_l V^{2/3} = K(T_C - T)$$



## Equilibrium Temperature Effect

- Noticed over long equilibrium tests; drift in  $\theta(T)$
- Substrate temperature ramp, static equilibrium droplet
  - Variation in  $\theta(T)$ , counter-intuitive
  - Temperature rises / Surface tension drops / Contact angle increases, greater change in adhesion tension



## Conclusion

Wetting properties measured on multiple EMIIIm / solid material combinations

- PTFE alone exhibits high resistance to wetting / adhesion / chemical reaction
- Pyrex / Tungsten easily wetted by EMIIIm
- Increase in surface roughness appears to increase rate of wetting
- Temperature decreases surface tension, ambiguous effect on wetting due to adhesion tension of the solid

## Future Work

- Repeat with other IL electrospray propellants
- Test more substrates, find a conductive solid with wetting properties similar to PTFE
- Include acid wash to clean substrate surface
- Reduce water content of EMIIIm via titration process, increase accuracy
- Test EMIIIm in electrospray at AFRL

## Acknowledgements

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- Dr. William Hargus, AFRL / RZSS Edwards AFB CA



